

EUR 2624.e

EUROPEAN ATOMIC ENERGY COMMUNITY — EURATOM

**A ONE-GROUP COLLISION PROBABILITY CODE
FOR CYLINDERS AND SLABS**

by

B. QUIQUEMELLE

1966



Joint Nuclear Research Center
Ispra Establishment — Italy
Reactor Physics Department
Reactor Theory and Analysis

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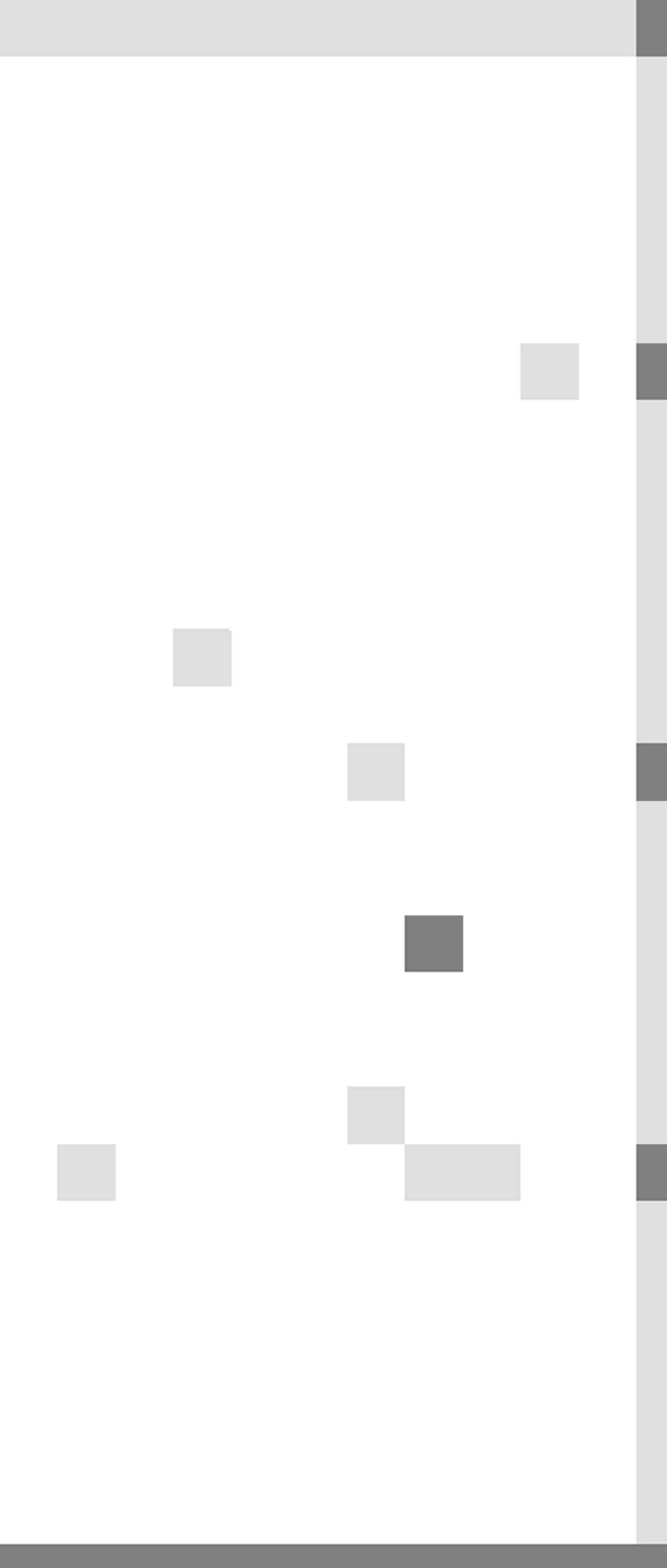
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Summary

The Code ^{XXXX} forms the numerical evaluation of the collision probabilities in concentric spheres or slabs. For cell calculations several boundary conditions can be included including a black inner region. Escape probabilities and Dancoff coefficients calculations are compared with other methods. The complete list of the FORTRAN programme is given.

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A one-group collision probability code for cylinders and slabs

Part I : Description of the method

Introduction (°)

In solving practical problems of neutron transport, the first flight collision probability theory has been proved successful since already some years. This theory provides a link between the most powerful methods for calculating the slowing down and the spatial distribution of neutrons.

Several works have dealt the analytical evaluation of collision probabilities in the simplest geometries. It has been thought interesting to solve the problem in using a straightforward numerical technique. Useful conclusions can then be drawn on the validity of such numerical techniques by comparison with the exact analytical evaluation

(°) Manuscript received on November 5, 1965

Method of Calculation

We will consider now a reactor or a lattice cell which can be represented by a one-dimensional geometry. Those geometries are formed of concentric cylinders or side by side slabs; also if we consider a regular lattice, the periodic structure will be taken into account by a suitable boundary condition.

We want to calculate the probability $P_{R_1 \rightarrow R_j}$ that a neutron born in a region "R₁" - with a given space-angle distribution - collides in a region "R_j". In case of a regular lattice, R₁ refers to a well defined region of the cell together with the homolog region in the other cells (through a suitable cell boundary condition).

Considering a normalized source of neutron in region "R₁" and the corresponding first flight collision flux ϕ , the quantity to be calculated is just

$$P_{R_1 \rightarrow R_j} = \int_{R_j} \phi(r) \Sigma_t(r) dr$$

where Σ_t is the total cross section at space point r.

Such a problem is easily solved by the numerical integration of the inhomogeneous Boltzmann equation using the so-called "S_n approximation". This approximation consists in the discretisation of the angular and space variables. A mesh cell is then specified by an index i for the space variable and two indices l,m for the direction of flight vector. One then considers¹ the value of the flux on each boundary of the mesh cell such as ϕ_i which is the value at space point r_i (or x_i) when the direction of flight is an averaged direction inside the mesh cell. Similar definitions¹ exist for ϕ_m and ϕ_l . A set of difference type equations is written between those values ϕ_i , ϕ_m and ϕ_l by representing the flux with an approximate shape inside the mesh cell.

In usual S_n calculations, this set is solved from mesh cell to mesh cell by starting with known conditions on the boundary of the system, then solving the equations by recursion and iterating until a conver-

gence criterium is reached. In our case we are interested in the collision probabilities for which the medium is considered to be absorbing for all types of collisions. Then no iteration is needed which avoid the most time consuming operations of the usual S_n .

Without going in any more details the main equations solved by the code have been gathered in appendix I.

If the calculation is done inside one cell of a lattice, the contributions from other cells are introduced through a balance equation at the external boundary

$$\vec{\Phi}_I = R \cdot (\vec{g}_I + T \cdot \vec{\Phi}_I)$$

The vectors have for components the flux along the discrete directions chosen for the mechanical quadrature. It is really this balance equation which avoids the iteration over the space mesh and which suppresses the need for the inner iteration of the usual S_n codes.

- \vec{g}_I represents the neutrons coming directly from the source and leaving the lattice cell without having collided.
 - $\vec{\Phi}_I$ represents the neutrons coming from the other cells in the lattice.
 - T is the transmission matrix of the lattice cell for incoming neutrons. When the set of discrete directions is symmetric for inward and outward directions this matrix is diagonal. In this case the elements of the matrix T are found in solving the system of equations of appendix I for an isotropic boundary source of unit intensity and collecting the number of neutrons leaving the cell along discrete outward directions.
- The elements of the matrix R represent the coefficients of transfer from one outward direction to one inward direction.

The result of the calculation is just a square matrix of the $P_{R_i \rightarrow R_j}$ which we will write more simply P_{ij} . The elements of this matrix must satisfy the reciprocity relations

$$V_i \lambda_j P_{ij} = V_j \lambda_i P_{ji}$$

and also the conservation relations (in an infinite lattice)

$$\sum_j P_{ij} = 1$$

where V and λ are the volume and mean free path inside the region designated by the subscript. It should be noted that those relations are already a very good check for the accuracy of the numerical method.

Conclusion

This method for calculating the collision probabilities is fast and accurate. When used for a lattice geometry, rather complicated boundary laws are simply introduced through the specification of the R matrix. In the present code the neutrons are started uniformly and isotropically in each region but an extension has been done for dealing with anisotropic sources¹⁴. This code can also be used like a subroutine for calculating transport kernels with a flux calculation method similar to the THERMOS method¹². It is thought that rather accurate kernels are found in a short time even for large size regions. The advantage of this method over the DSN method is that the S_n approximation is used only for calculating accurate transport kernels with a minimum effort, then well developed techniques for accelerating convergence are used to solve the linear flux equations¹².

List of Symbols

i	index for designation of a space mesh boundary
l, m	two indices for designation of an angular mesh boundary
ϕ_k	($k = i, l$ or m) value of the flux on the boundary labelled by index k when the variables which varies over other boundaries have a mean value ³
\sum_i	total cross section inside space mesh r_i, r_{i+1}
w	weight associated to the discrete direction inside the mesh cell and used for mechanical quadrature (half value indices are generally omitted for clarity)
μ	direction cosine
r_i, r_{i+1}	inner and outer radius of mesh i in cylindrical geometry
x_i, x_{i+1}	abscissa defining the mesh i in slab geometry
$P_{R_i \rightarrow R_j}$	probability that a neutron born uniformly and isotropically in region R_i suffers his first collision in region R_j
δ_R	is 1 inside the region R and 0 outside
I	number of space mesh
n	order of approximation for the discrete angular representation In cylindrical geometry there exist $\frac{n(n+4)}{4}$ discrete directions and in slab geometry there exist n discrete directions.

Part 2: Some applications of the code
=====

The code has been applied to a variety of problems and results were compared with exact methods.

a) calculation of escape probabilities:

We consider, by example, a two-media cell in a lattice consisting of a fuel rod surrounded by a moderator. The probability of escaping the rod is just

$$P_o = P_{f \rightarrow m}$$

where $P_{f \rightarrow m}$ is calculated using the code TIJ with two regions (fuel + moderator). Such a calculation is reported in table II and compared with other analytical methods. It should be noted that the best boundary condition is given by an isotropic return along directions which have the same azimuth that the incident neutron direction (although the difference with a purely isotropic return is negligible). In this case the results compared very closely with the analytic calculations of Pennington⁴. We can also state that there exists no simple specification for finding the exact results of Fukai⁵ with any combination of two or three boundary laws.

In table III a similar calculation was performed and shows a very good agreement with Monte Carlo calculations reported by Rothenstein⁷.

Table II

Escape Probabilities

(a (radius of rod) = 0.183 inch, $v_m/v_f = 1.0$, $\sum_m = 1.49170 \text{ cm}^{-1}$)

\sum_{fuel}^a	Takahashi ⁶	TIJ			Pennington ⁴	exact ⁵
		IBVL = 1	IBVL = 3	IBVL = 2		
0.1	0.76875	0.7723	0.8160	0.8157	0.81364	0.80745
0.3	0.52590	0.5295	0.5908	0.5898	0.58855	0.57988
0.5	0.39776	0.4014	0.4589	0.4575	0.45695	0.44745
0.8	0.28918	0.2927	0.3400	0.3383	0.33839	0.32973
1.0	0.24372	0.2471	0.2884	0.2886	0.28694	0.27918
2.0	0.12393	0.1358	0.1603	0.1588	0.15912	0.15490
4.0	0.068981	0.07047	0.08281	0.08196	0.082044	0.080363

* approximation S_{16}

IBVL = 1 (mirror reflection)

IBVL = 3 (white boundary)

IBVL = 2 (isotropic return along same azimuth)

Table III

Escape Probabilities

$$(v_m/v_f = 1.0, \sum_m = 1.4916 \text{ cm}^{-1})$$

\sum_{fuel}^a	TIJ*	Monte Carlo ⁷	TIJ*	Monte Carlo ⁷
0.5	0.5750 (0.5631)	0.572 (0.553)	0.6950	0.691
1.0	0.3988	0.397	0.5243 (0.5159)	0.522 (0.513)
1.458	-	-	0.4237	0.422
1.5	0.3026 (0.2909)	0.304 (0.291)	-	-
2.0	0.2424	0.248	0.3422 (0.3343)	0.346 (0.335)
3.0	0.1718 (0.1636)	0.173 (0.163)	0.2491	0.250
4.0	0.1324	0.133	0.1939 (0.1883)	0.194 (0.190)
6.0	0.09017 (0.0851)	0.088 (0.082)	0.1330	0.133
8.0	-	-	0.1007 (0.0976)	0.100 (0.099)
	a = 0.25 inch		a = 0.60 inch	

* approximation S_{16} with isotropic return
 (values between parenthesis include the effect of a 0.33 in. cladding)

b) Dancoff factor calculations

It is possible to specify a black inner region in the cylindrical geometry. In this case TIJ code prints the current J_{in}^- of neutrons entering the black region. If we perform a two region calculation with a cell boundary condition (IBVL different of 0) we can calculate the shadowing factor of Dancoff:

$$C = J_{in}^- \times 4 \sum_m$$

where $1/4 \sum_m$ is the current in the infinite moderator.

Such a calculation is reported on table IV and compared to exact Monte Carlo⁸ calculations. There is a maximum discrepancy of 3.5% which can well be explained by the inadequacy of the linear approximation near the inner black boundary. It should be also necessary to use more discrete directions near the discontinuity of the angular flux at the black boundary. Those calculations compare well with some analytical results⁹ but they are not as accurate as the Sauer¹⁰ approximation.

Table IV

Dancoff coefficient

$$\left(\sum_m = 1.4916 \right)$$

Rod size (inch)	V_m/V_f	IBVL = 1	TIJ IBVL = 2	IBVL = 3	Monte Carlo ⁸
0.250	1.0	0.4532	0.5507	0.5400	0.52690
	1.5	0.5637	0.6797	0.6718	0.64627
	2.0	0.6342	0.7551	0.7472	0.73077
	3.0	0.7366	0.8514	0.8445	0.82361
	4.0	0.8026	0.9040	0.8983	0.88566
0.387	1.0	0.5960	0.6898	0.6820	0.66169
	1.5	0.7071	0.8023	0.7949	0.77261
	2.0	0.7751	0.8678	0.8619	0.84533
	3.0	0.8670	0.9357	0.9309	0.90732
	4.0	0.9252	0.9729	0.9697	0.95422
0.600	1.0	0.7446	0.8186	0.8113	0.78285
	1.5	0.8434	-	0.8992	-
	2.0	0.9005	0.9487	0.9444	0.92802
	3.0	0.9567	0.9854	0.9829	0.95930
	4.0	0.9817	0.9989	0.9975	0.99876

All previous calculations have been done with the S_{16} approximation. This is a rather high approximation which is not necessary in most cases. On table V the escape probabilities of table II have been evaluated as a function of the order of approximation. For practical purpose it is concluded that the approximation S_4 would be sufficient in this case.

It is anticipated that when used with a multigroup thermalization code TIJ would compute the 30-group transport kernels in a time of about one minute (IBM 7094) for a two region cell as above with the approximation S_4 .

Table V

Escape Probabilities Against Order of Approximation
(see table II)

$\sum_g a$	S_2	S_4	S_6	S_8	S_{12}	S_{16}
0.1	0.8334	0.8204	0.8189	0.8178	0.8166	0.8160
0.3	0.6184	0.5965	0.5946	0.5932	0.5916	0.5908
0.5	0.4869	0.4641	0.4624	0.4611	0.4597	0.4589
0.8	0.3650	0.3446	0.3431	0.3420	0.3407	0.3400
1.0	0.3113	0.2927	0.2913	0.2902	0.2890	0.2884

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Appendix 1

Summary of main equations

1) Cylindrical geometry

difference equation for boundary values

$$\mu (r_{m+1} \phi_{m+1} - r_i \phi_i) - \frac{r_{m+1} - r_i}{\ell} (\gamma_{m+1} \phi_{m+1} - \gamma_m \phi_m) +$$

$$\frac{r_{m+1} - r_i}{6} \sum_i \left[(\ell r_{m+1} + r_i) \phi_i + (\ell r_i + r_{m+1}) \phi_{i+1} \right] = \int_R \frac{r_{i+1}^2 - r_i^2}{\ell}$$

recursion relation for the coefficients of streaming between rays

$$\gamma_{m+1} - \gamma_m = \ell \mu w \quad (\gamma_0 = 0)$$

linear approximation for the shape of the flux inside a mesh cell

$$\phi_{i+1} + \phi_i = \phi_{m+1} + \phi_m = \ell \bar{\phi}_i$$

$$\begin{array}{ll} i = 1, 2, 3 \dots & I+1 \\ m = 1, 2 \dots & n-2(\ell-1) \\ \ell = 1, 2 \dots & \frac{n}{2} \end{array}$$

for $m = 0$ the following difference equation is used:

$$\mu (r_{i+1} + r_i) (\phi_{i+1} - \phi_i) +$$

$$\frac{r_{i+1} - r_i}{6} \sum_i \left[(\ell r_{i+1} + r_i) \phi_i + (\ell r_i + r_{i+1}) \phi_{i+1} \right] = \int_R \frac{r_{i+1}^2 - r_i^2}{\ell}$$

and

$$\phi_i + \phi_{i+1} = \ell \phi_{m=0}$$

2) Slab geometry

difference equation

$$\mu (\phi_{i+1} - \phi_i) + \frac{\sum_i (X_{i+1} - X_i)(\phi_{i+1} + \phi_i)}{2} = \int_R (X_{i+1} - X_i)$$

approximation (same as in cylindrical geometry)

$$i = 1, 2 \dots I+1$$

$$m = 1, 2 \dots n$$

3) Both geometries

$$\phi(i) = \sum_{m,p} w \bar{\phi}$$

(total flux)

$$P_{R \rightarrow R'} = \frac{1}{V_R} \sum_{i \in R'} (\phi \Sigma_t V)_i$$

(collision probability)

Appendix 2

=====

Input data format

card 1

col 2-72

identification of the problem

card 2

(FORMAT 2413)

col 1-3 (ISN)

n = 2,4,6,8,12 or 16

col 4-6 (IGEOM)

o slab geometry

1 cylindrical geometry

col 7-9 (ICVL)

condition at r (or x) = 0

- cylindrical geometry

o the inner region is a black region

1 reflective condition

- slab geometry

1 reflective condition

2 periodicity condition

col 10-12 (IBVL)

condition at the outer boundary

- cylindrical geometry (r = r₁)

o the system is in void

1 mirror reflection condition

2 isotropic return along directions of same azimuth

3 isotropic return along all directions

4 arbitrary input law of reflection

- slab geometry

1 mirror reflection (if ICVL = 2 then the periodicity condition is applied)

col 13-15	IAPPT	
16-18	ITSNPT	
19-21	IBVLPT	printing options
22-24	ICVLPT	(see list of symbols in appendix 4)
25-27	ITPT	
28-30	ISNPT	

card 3 (FØRMAT 2I3)

col 1-3	(NR)	nb of regions
col 4-6	(NMAT)	nb of cross sections

card 4 (FØRMAT 24I3)

col 1-3 etc...	nb of cross section inside each consecutive region
----------------	--

card 5 (FØRMAT 6E12.5)

col 1-12 etc...	1	cross section nb 1
	2	" 2
	NMAT	" NMAT

(as much card as necessary)

card 6 (FØRMAT 6E12.5)

col 1-12 etc...	t_1	thickness of region 1
	t_2	" 2
	t_{NR}	" NR

(as much card as necessary)

card 7 (FØRMAT 6E12.5)

col 1-12	a = 10.0	
13-124	b = 2.0	(see subroutine MESH)
25-36	c = 1.0	

next problem follows

Appendix 3

Sample Problem

The sample problem corresponds to the case calculated by Jonsson¹³
We consider a three-region system with radii of 1, 2 and 3 mean free
path. Results are given in following table.

P_{ij} i j	T_{ij} (IBVL = 2)	Theseus ¹³
1 1	0.5915	0.5929
1 2	0.3012	0.3005
1 3	0.0740	0.0732
2 1	0.1002	0.1002
2 2	0.6190	0.6239
2 3	0.2122	0.2112
3 1	0.0148	0.0147
3 2	0.1271	0.1267
3 3	0.6112	0.6168

SAMPLE PROBLEM FOR
 Tij
 (A ONE GROUP TRANSMISSION PROBABILITY
 CODE FOR CALCULATING
 GEOMETRIES)

SAMPLE PROBLEM (JONSSON J. OF NUC. EN. VOL 17 P. 515)

16 1 1 0

3 1

1 1 1

1.0

1.0

10.0

1.0

2.0

1.0

1.0

CARD

1

2

3

4

5

6

7

* XEQ

ENTRY POINTS TO SUBROUTINES REQUESTED FROM LIBRARY,
(FPT) (TSM) (RTN) (STHM) (FIL) EXIT SQRT

EXECUTION
SAMPLE PROBLEM OF TIJ(A ONE-DIMENSIONAL COLLISION PROBABILITY CODE)

APPROXIMATION S 16

IGEOM= 1

ICVL = 1

IBVL = 0

	THICKNESS	MATERIAL	SIGMA-TOT
	1	2	3
1	0.10000E 01	1	0.10000E 01
2	0.10000E 01	1	
3	0.10000E 01	1	

MATRIX PIJ*LAMDAJ*VI

	1	2	3
1	0.29574E-00	0.15061E-00	0.37004E-01
2	0.15031E-00	0.92854E 00	0.31837E-00
3	0.37126E-01	0.31785E-00	0.15279E 01

VOLUME OF REGICNS

	1
1	0.50000E 00
2	0.15000E 01
3	0.25000E 01

COLLISION PROBABILITY MATRIX

	1	2	3
1	0.59148E 00	0.30123E-00	0.74008E-01
2	0.10021E-00	0.61903E 00	0.21224E-00
3	0.14850E-01	0.12714E-00	0.61118E 00

32 LINES OUTPUT THIS JOB.

JOB START AT 20.50
COMP./LOAD TIME 00.008
EXECUTION TIME 00.003
TOTAL JOB TIME 00.011

Appendix 4

=====

List of symbols with printing
option

Fortran name	Variable name* or description	Printing option
DMU (M,L)	(direction cosine)	ISNPT
W (M,L)	w (weight for quadrature)	ISNPT
F(M,L)	Diagonal elements of matrix T (boundary transparence coefficients)	ISNPT
CVL(M,L)	Angular flux at center	ICVLPT
BVL(M,L)	Angular flux at boundary and \vec{g}_L vector components	IBVLPT
PTTP(ML,ML)	Elements of reflection matrix R (direc- tions are ordered like in ref. 2 p. 13)	ISNPT
BVLZW(L)	Angular flux at boundary along $m = 0$ directions (zero weight directions)	IBVLPT
TH(I)	thickness of regions)	always printed
SGT(I)	cross section) see input data	
IMAT(I)	material table) specifications	
T(I,J)	$P_{R_i \rightarrow R_j}$	ITPT
R(I)	r_i, x_i	ITSNPT

*
refer to text

DR(I)	$r_{i+1} - r_i, x_{i+1} - x_i$	ITSNPT
RM(I)	$\frac{r_{i+1} + r_i}{2}, \frac{x_{i+1} + x_i}{2}$	ITSNPT
V(I)	$\frac{r_{i+1}^2 - r_i^2}{2}, x_{i+1} - x_i$	ITSNPT
VNR(I)	volume of regions	ITSNPT
FMT(I)	ϕ_i	IAPPT
BM(I)	ϕ_m	IAPPT
TSN(I)		ISNPT

Appendix 5

Description of the subroutines

1) TIJ (main routine)

- read input data
- set up the elements of the R matrix if IBVL \neq 0, 1, 4
- monitor the complete calculation

2) Subroutine CYL (ARG1, ARG2, ARG3)

This routine solves the equations of table I and has two calling sequences:

- a) CALL CYL (IR, ISL, ISR) then an uniform and isotropic source is placed in region IR which means between mesh points r_{ISL+1} (or x_{ISL+1}) and r_{ISR} (or x_{ISR}). The flux is stored in vector TSN (direct transfer) and components of vector g are collected.
- b) CALL CYL (0, IMAXI, IMAXI) then no source is introduced but the boundary flux found in the data block BVL is imposed at the external surface. The flux value are cumulated in TSN (total transfer).

3) Subroutine DMND

From appendix I this subroutine calculates:

- ϕ_i function of ϕ_m, ϕ_{i+1} for inward directions
- ϕ_{i+1} function of ϕ_m, ϕ_i for outward directions

4) Subroutine ZWGHT (Y)

is used in cylindrical geometry for the directions ($m=0$) which cross the axis of the cylinder.

$$2 Y = (\phi_i + \phi_{i+1})_{m=0}$$

5) Subroutine BVLCYL

solves the balance equation at the boundary of the lattice cell in cylindrical geometry.

When IBVL is different of 0 or 1, the equation is solved after a fixed number (11) of successive substitutions.

6) Subroutine SLABBC

applies boundary condition on each discrete direction in a slab geometry

7) Subroutine TKRNL(IR)

sets up the collision probability matrix elements when the source region is IR. Also it computes $\sum_{\phi} P_{ij}$ which must sum to one if the boundary la conserves neutrons and is symmetrical.

8) Subroutine SNWGT

prepares μ and w for each discrete directions. The three direction cosines are taken from the set of n/2 values.

$$\mu_m^2 = \frac{6m - 5}{3(n-1)} \quad m = 1, 2 \dots \frac{n}{2}$$

The weights are those calculated by Lee² using the area method.

9) Subroutine MESH

A fine mesh is automatically prepared. In each region i, the mesh size is λ_{i1}/A with a minimum of B mesh interval in each region (A and B are input data). C is used to modify the mesh size within C mean free path of a boundary.

10) Subroutine MATPT (A, IDIM, JDIM, KDIM, I, J, K)

prints automatically in a suitable form a matrix A with one, two or three dimension (see code for use).

11) Subroutine VCTRPT (N, V1, I1, F1, ..., VN, IN, FN)

prints vector of dimension I with variable format

F = 2 (floating point format)

F = 1 (integer point format)

12) Subroutine RLINK

13) Subroutine PRINT

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* LABEL
CTIJ000
DIMENSION CMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)T1J00001
11,BVLZW(8) T1J00002
DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20) T1J00003
DIMENSION R(500),CR(500),V(500),RM(500),SGTV(500),BM(500),FMT(500)T1J00004
11,TSN(500) T1J00005
CCMNCNICEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTCUT T1J00006
CCMCONK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4 T1J00007
CCMCONWRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,B1,S T1J00008
CCMCONCMU,W,F,CVL,BVL,PTTP T1J00009
CCMCONTH,SGT,IMAT,NMSH,T T1J00010
CCMCONR,CR,V,RM,SGTV,BM,FMT,TSN,BVLZW T1J00011
CCMCONISNHIC,ISNH1,ISN1,ISNHG,ICVL,IBVL,IBLCK,NRINIT,PI T1J00012
CCMCONIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNPT T1J00013
NTIN=5 T1J00014
NTOUT=6 T1J00015
PI=3.1415927 T1J00016
10 ISNO=ISN T1J00017
READ INPUT TAPE NTIN,6 T1J00018
WRITE OUTPUT TAPE NTCLT,6 T1J00019
READINPUPTTAPENTIN ,1,ISN,IGEOM,ICVL,IBVL,IAFPT,ITSNPT,IBVLPT,ICVLPT T1J00020
11,ITPT,ISNPT T1J00021
WRITE OUTPUT TAPE NTCLT,5,ISN,IGEOM,ICVL,IBVL T1J00022
IF(ISNO-ISN)15,20,15 T1J00023
15 ISNH=ISN/2 T1J00024
ISNH1G=ISNH+1+IGEOM T1J00025
ISNH1=ISNH+1 T1J00026
ISN1=ISN+1 T1J00027
ISN1G=ISN+1+IGEOM T1J00028
ISNHG=ISNH+IGEOM T1J00029
ISNG=ISN+IGEOM T1J00030
CALLSNWCT T1J00031
20 READ INPUT TAPE NTIN,1,NR,NMAT T1J00032
READ INPUT TAPE NTIN,1,(IMAT(I),I=1,NR) T1J00033
READ INPUT TAPE NTIN,3,(SGT(I),I=1,NMAT) T1J00034
READ INPUT TAPE NTIN,3,(TH(I),I=1,NR) T1J00035
WRITE OUTPUT TAPE NTCLT,4 T1J00036
CALLVCTRPT(3,TH,NR,2,IMAT,NR,1,SGT,NMAT,2) T1J00037
CALLMESH T1J00038
CC50LC=1,ISNH T1J00039
CC50MC=1,ISN1 T1J00040
50 F(MC,LC)=0.0 T1J00041
IF(IGEOM)300,300,100 T1J00042
C CALCULATION OF TRANSPARENCY COEFFICIENTS FOR CYLINDER T1J00043
100 DC 150 I=1,IMAX1 T1J00044
150 TSN(I)=C.0 T1J00045
CC8000LC=1,ISNH T1J00046
J1=ISNH1G-LC T1J00047
CC8000MC=1,J1 T1J00048
8000 BVL(MC,LC)=1.0 T1J00049
CALLCYL(0,IMAX1,IMAX1) T1J00050
IF(IBVLPT)8200,8200,8100 T1J00051
8100 WRITECUTPUTTAPENTCUT,2001 T1J00052
CALL MATPT(PVL,17,8,1,ISN1,ISNH,1) T1J00053
8200 CC8500LC=1,ISNH T1J00054
F(1,LC)=BVLZW(LC) T1J00055
J1=ISNH1G-LC T1J00056
CC8500MC=2,J1 T1J00057
MP=2*J1+1-MC T1J00058
8500 F(MC,LC)=BVL(MP,LC) T1J00059
IF(ITSNPT)8600,8600,8550 T1J00060
8550 WRITECUTPUTTAPENTCUT,3000 T1J00061
CALL MATPT(F,17,8,1,ISNHG,ISNH,1) T1J00062
8600 K1=ISN*(ISN+2) T1J00063
K1=K1/8 T1J00064
IF(1BVL-4)154,152,154 T1J00065
154 IF(1BVL-1)370,370,175 T1J00066
152 DC 153 K2=1,K1 T1J00067
153 READ INPUT TAPE NTIN,3,(PTTP(K2,K),K=1,K1) T1J00068
170 IF(ITSNPT)370,370,171 T1J00069
171 WRITECUTPUTTAPENTCUT,5000 T1J00070
CALLMATPT(PTTP,36,36,1,K1,K1,1) T1J00071
GCTC370 T1J00072
175 IF(1BVL-2)999,176,185 T1J00073
176 MCLC=0 T1J00074
DC180LC=1,ISNH T1J00075
J2=ISNH1G-LC+1 T1J00076
J3=ISNH-2(LC-1) T1J00077
WRK1=0.0 T1J00078
CC178MC=J2,J3 T1J00079
178 WRK1=WRK1+W(MC,LC)*CMU(MC,LC) T1J00080
K2=MCLC+1 T1J00081
K3=MCLC+ISNH-1-LC T1J00082

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	CC180 MC=J2,J3	TIJ00083
	MCLC=MCLC+1	TIJ00084
	WPL=W(MC,LC)	TIJ00085
	DMUML=DMU(MC,LC)	TIJ00086
	CC180K=K2,K3	TIJ00087
180	PTTP(K,MCLC)=DMUML*WPL/WRK1	TIJ00088
	GCTO170	TIJ00089
185	MCLC=0	TIJ00090
	WRK1=0.0	TIJ00091
	CC188LC=1,ISNH	TIJ00092
	J1=ISNH1G-LC	TIJ00093
	CC188MC=1,J1	TIJ00094
188	WRK1=WRK1+W(MC,LC)*DMU(MC,LC)	TIJ00095
	CC190LC=1,ISNH	TIJ00096
	J2=ISNH1G-LC+1	TIJ00097
	J3=ISNH2*(LC-1)	TIJ00098
	CC190MC=J2,J3	TIJ00099
	MCLC=MCLC+1	TIJ00100
	WPL=W(MC,LC)	TIJ00101
	DMUML=DMU(MC,LC)	TIJ00102
	CC190K=1,K1	TIJ00103
190	PTTP(K,MCLC)=DMUML*WPL/ABS(F(WRK1))	TIJ00104
	GCTO170	TIJ00105
C	CALCULATION OF TRANSPARENCY COEFFICIENTS FOR SLAB	TIJ00106
300	CC355MC=1,ISNH	TIJ00107
	DMUML=DMU(MC,1)	TIJ00108
	BI=1.0	TIJ00109
	CC350I=1,IMAX	TIJ00110
	I1=IMAX1-I	TIJ00111
350	CALLCMNC	TIJ00112
355	F(MC,1)=BI	TIJ00113
360	IF(1)370,370,365	TIJ00114
365	WRITECUTPUTTAPENTCUT,3000	TIJ00115
	CALLVCTRPT(1,F,ISNH1G,2)	TIJ00116
370	CC400I=1,NR	TIJ00117
	CC400J=1,NR	TIJ00118
400	T(I,J)=0.0	TIJ00119
	ISR=0	TIJ00120
	ISL=0	TIJ00121
	IF(1)410,410,415	TIJ00122
410	IF(1)415,415,412	TIJ00123
412	NRINIT=2	TIJ00124
	GCTO420	TIJ00125
415	NRINIT=1	TIJ00126
420	CC600IR=NRINIT,NR	TIJ00127
	CC450LC=1,ISNH	TIJ00128
	CC450MC=1,ISNH	TIJ00129
	CVL(MC,LC)=0.0	TIJ00130
450	BVL(MC,LC)=0.0	TIJ00131
	CC460I=1,IMAX1	TIJ00132
460	TSN(I)=0.0	TIJ00133
	CTIM=0.0	TIJ00134
	ISR=ISR+NMSH(IR)	TIJ00135
	ISL=ISL-NMSH(IR)	TIJ00136
	CALLCYL(IR,ISL,ISR)	TIJ00137
462	CC463LC=1,ISNH	TIJ00138
	J1=ISNH1G-LC	TIJ00139
	CC4620MC=1,J1	TIJ00140
4620	CTIM=CTIM+CVL(MC,LC)*W(MC,LC)*DMU(MC,LC)	TIJ00141
	J2=J1+1	TIJ00142
	J3=2*J1-IGECM	TIJ00143
463	CONTINUE	TIJ00144
464	ISL1=ISL+1	TIJ00145
	IF(1)470,470,465	TIJ00146
465	WRITECUTPUTTAPENTOUT,2000,ISL1,ISR	TIJ00147
	WRITECUTPUTTAPENTOUT,2002	TIJ00148
	CALLVCTRPT(1,TSN,IMAX1,2)	TIJ00149
470	IF(1)480,480,475	TIJ00150
475	WRITECUTPUTTAPENTOUT,2001	TIJ00151
	CALL MATPT(BVL,17,8,1,ISNH,ISNH,1)	TIJ00152
480	IF(1)500,500,520	TIJ00153
500	CALLSLAABC	TIJ00154
	GCTO560	TIJ00155
520	IF(1)550,550,550	TIJ00156
550	CALLBVL CYL	TIJ00157
560	CALLCYL(0,IMAX1,IMAX1)	TIJ00158
562	CC563LC=1,ISNH	TIJ00159
	J1=ISNH1G-LC	TIJ00160
	CC1562MC=1,J1	TIJ00161
1562	CTIM=CTIM+CVL(MC,LC)*W(MC,LC)*DMU(MC,LC)	TIJ00162
	J2=J1+1	TIJ00163
	J3=2*J1-IGECM	TIJ00164
563	CONTINUE	TIJ00165
2563	IF(1)564,564,564	TIJ00166

1563	WRITE CLTPUT TAPE 6,5001,CTIM	TIJ00167
564	IF(ITSNPT)570,570,565	TIJ00168
565	WRITECUTPUTTAPENTOUT,2000,ISL1,ISR	TIJ00169
	WRITECUTPUTTAPENTOUT,2003	TIJ00170
	CALLVCTRPT(1,TSN,IMAX1,2)	TIJ00171
570	IF(IBVLPT)580,580,575	TIJ00172
575	WRITECUTPUTTAPENTOUT,2001	TIJ00173
	CALLMATFT(BVL,17, 8,1,ISNG,ISNH,1)	TIJ00174
580	CALLTKRNL(IR)	TIJ00175
600	CCNTIAUE	TIJ00176
999	GCTO10	TIJ00177
	1 FCRMAT(24I3)	TIJ00178
	3 FCRMAT(6E12.5)	TIJ00179
	4 FCRMAT(1H09X37HTHICKNESS MATERIAL SIGMA-TOT)	TIJ00180
	5 FCRMAT(16H0APPROXIMATION S,13/7H0IGECM=[13/7H0ICVL =13/7H0IBVL =13/7H0I	TIJ00181
	1)	TIJ00182
	6 FCRMAT(72H	TIJ00183
	1	TIJ00184
2000	FCRMAT(1H08X11HSOURCE(I)=1/10X3H(I=I2,1H,I2,1H))	TIJ00185
2002	FCRMAT(1H07X15HDIRECT TR.COE.F.)	TIJ00186
2001	FCRMAT(23H0BOUNDARY VALUES MATRIX)	TIJ00187
2003	FCRMAT(1H07X14HTOTAL TR.COE.F.)	TIJ00188
3000	FCRMAT(35H0BOUNDARY TRANSPARENCE COEFFICIENTS)	TIJ00189
4001	FCRMAT(1H0)	TIJ00190
5000	FCRMAT(18H0REFLECTION MATRIX)	TIJ00191
5001	FCRMAT(27H0CURRENT AT BLACK BOUNDARY=E12.5)	TIJ00192
	ENC	TIJ00193
*	LABEL	
CCYL000		CYL00000
	SLBRoutineCYL(IR,ISL,ISR)	CYL00001
	DIMENSION CMU(17,8),w(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)	CYL00002
	1),BVLZW(8)	CYL00003
	DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	CYL00004
	DIMENSION R(500),CR(500),V(500),RM(500),SGTHV(500),RM(500),FMT(500)	CYL00005
	1),TSN(500)	CYL00006
	COMMONICEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT	CYL00007
	COMMONK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4	CYL00008
	COMMONWRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,BI,S	CYL00009
	COMMONCMU,w,F,CVL,BVL,PTTP	CYL00010
	COMMONTH,SGT,IMAT,NMSH,T	CYL00011
	COMMONCR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW	CYL00012
	COMMONISNHIC,ISNH1,ISN1,ISNIG,ICVL,IBVL,IPLCK,NRINIT,PI	CYL00013
	COMMONIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNPT	CYL00014
	DC4COLC=1,ISNH	CYL00015
	DC20I=1,IMAX1	CYL00016
	BM(I)=0.0	CYL00017
20	FMT(I)=0.0	CYL00018
	GMP=0.0	CYL00019
	GMP1=0.0	CYL00020
C	INWARD DIRECTIONS MESH SWEEP	CYL00021
	J1=ISNHIG-LC	CYL00022
	DC2COMC=1,J1	CYL00023
	WML=W(MC,LC)	CYL00024
	DMUML=CMU(MC,LC)	CYL00025
75	IF(IGECM)85,85,80	CYL00026
80	GMP=GMP1	CYL00027
	GMP1=CMF1-2.0*WML*DMUML	CYL00028
85	IF(IR)90,90,99	CYL00029
90	BI=BVL(MC,LC)	CYL00030
	IM=IMAX	CYL00031
	GCTC100	CYL00032
99	BI=0.0	CYL00033
	IM=IMAX	CYL00034
100	TSN(IM+1)=TSN(IM)+WML*BI	CYL00035
	FMT(IM+1)=BI	CYL00036
	DC150I=1,IM	CYL00037
	I1=IM-I+1	CYL00038
	I2=I1	CYL00039
	IF(I1-ISL)110,110,113	CYL00040
113	IF(I1-ISR)112,112,110	CYL00041
112	S=1.0	CYL00042
	GCTC115	CYL00043
110	S=0.0	CYL00044
115	IF(WML)120,120,130	CYL00045
120	CALLZKGF(Y)	CYL00046
	BM(I1)=Y	CYL00047
	GCTC150	CYL00048
130	CALLCMND	CYL00049
	TSN(I2)=TSN(I2)+WML*FMT(I2)	CYL00050
150	CCNTINLE	CYL00051
152	IF(IAFPT)190,190,155	CYL00052
155	WRITECUTPUTTAPENTOUT,1000,MC,LC	CYL00053
	CALLVCTRPT(2,FMT,IMAX1,2,BM,IMAX,2)	CYL00054
190	CVL(MC,LC)=BI	CYL00055

192	IF(IWML)1920,1920,194	CYL00056
1920	IF(ICVL)1921,1921,1930	CYL00057
1921	BI=0.0	CYL00058
1930	CC196C11=1,IMAX	CYL00059
	I2=11+1	CYL00060
	IF(I1-ISL)1950,1950,1935	CYL00061
1935	IF(I1-ISR)1940,1940,1950	CYL00062
1940	S=1.0	CYL00063
	GCTC1955	CYL00064
1950	S=0.0	CYL00065
1955	CALLZWCHT(Y)	CYL00066
	FMT(11)=Y	CYL00067
1960	CCONTINUE	CYL00068
	BVLZW(LC)=81	CYL00069
	IF(IAFPT)200,200,1961	CYL00070
1961	WRITECUTPUTTAPENTOUT,4000	CYL00071
	CALLVCTRPT(1,FMT,IMAX,2)	CYL00072
	GCTC200	CYL00073
194	IF(IGECM)200,200,195	CYL00074
195	MF=2*J1+1-MC	CYL00075
	IF(ICVL)196,196,197	CYL00076
196	CVL(MP,LC)=C.0	CYL00077
	GOTC200	CYL00078
197	CVL(MP,LC)=F1	CYL00079
200	CCONTINUE	CYL00080
260	J2=J1+1	CYL00081
	J3=2*J1-IGECM	CYL00082
	CC390MC=J2,J3	CYL00083
	WML=W(MC,LC)	CYL00084
	DMUML=DMU(MC,LC)	CYL00085
264	IF(IGECM)265,265,270	CYL00086
265	IF(IR1275,275,267	CYL00087
267	BI=C.C	CYL00088
	IMIN=ISL+1	CYL00089
	GCTC280	CYL00090
270	GMP=GMP1	CYL00091
	GMP1=GMP1-2.0*WML*DMUML	CYL00092
275	IMIN=1	CYL00093
	BI=CVL(MC,LC)	CYL00094
280	TSN(IMIN)=TSN(IMIN)+WML*BI	CYL00095
	FMT(IMIN)=BI	CYL00096
	CC350I1=IMIN,IMAX	CYL00097
	I2=11+1	CYL00098
304	IF(I1-ISL)320,320,305	CYL00099
305	IF(I1-ISR)310,310,320	CYL00100
310	S=1.0	CYL00101
	CCTC330	CYL00102
320	S=0.0	CYL00103
330	CALLDMNC	CYL00104
335	TSN(I2)=TSN(I2)+WML*FMT(I2)	CYL00105
350	CONTINUE	CYL00106
356	IF(IAFPT)380,380,357	CYL00107
357	WRITECUTPUTTAPENTOUT,1000,MC,LC	CYL00108
	CALLVCTRPT(2,FMT,IMAX1,2,8M,IMAX,2)	CYL00109
380	BVL(MC,LC)=E1	CYL00110
390	CCONTINUE	CYL00111
	IF(IGECM)410,410,400	CYL00112
400	CCONTINUE	CYL00113
	J1=ISNH	CYL00114
	GCTC415	CYL00115
410	J1=1	CYL00116
415	IF(ICVLFT)450,450,420	CYL00117
420	WRITECUTPUTTAPENTOUT,2000	CYL00118
	CALLMATPT(CVL,17,8,1,ISN1,J1,1)	CYL00119
450	IF(IBVLFT)460,460,455	CYL00120
455	WRITECUTPUTTAPENTOUT,3000	CYL00121
	CALLVCTRPT(1,BVLZW,ISNH,2)	CYL00122
460	RETURN	CYL00123
1000	FORMAT(1H013X12HANGULAR FLUX/14X4H (M=12,4H,L= 12,1H)/1H011X3H NI1	CYL00124
	11X4HNM+1)	CYL00125
2000	FORMAT(22HOCENTRAL VALUES MATRIX)	CYL00126
3000	FORMAT(28HZERO WEIGHT BOUNDARY VALUES//)	CYL00127
4000	FORMAT(20HORADIAL OUTWARD FLUX//)	CYL00128
	END	CYL00129
*	LABEL	
CCMNDOO		CMND0000
	SUBROUTINECMNC	CMND0001
	DIMENSION CMU(17,8),W(17,2),F(17,2),CVL(17,8),BVL(17,8),PTTP(36,36	CMND0002
	1),BVLZW(2)	CMND0003
	DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	CMND0004
	DIMENSION R(500),CR(500),V(500),RV(500),SCTHV(500),BM(500),FMT(500	CMND0005
	1),TSN(500)	CMND0006
	COMMONIGECM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT	CMND0007
	COMMONK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4	CMND0008

	CCMNCNWRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,BI,S	CMND0009
	CCMONDMU,W,F,CVL,BVL,PTTP	CMND0010
	CCMNCNTH,SGT,IMAT,NMSH,T	CMND0011
	CCMNCNR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW	CMND0012
	CCMNCNISHIG,ISNH1,ISN1,ISN1G,ICVL,IBVL,IBLCK,NRINIT,PI	CMND0013
	CCMNCNIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNFT	CMND0014
50	IF(IIGECM)220,220,100	CMND0015
C	CALCULATES ANGULAR TERMS FOR CYLINDER	CMND0016
100	BM11=BM(11)	CMNC0017
	WRK3=CR(11)/WML/2.0	CMND0018
	WRK2=CMP1*WRK3	CMND0019
	WRK1=(CMP+GMP1)*WRK3*BM11/2.0	CMNC0020
	WRK4=SGT-V(11)/(6.0*RM(11))	CMNC0021
120	FM=(S*V(11)/2.0+BI*(ABSF(DMLML)*RM(11)+SIGNF(CR(11),CMUML)*WRK4)	CMND0022
	1+WRK1)/(4.0*WRK4*RM(11)+(ABSF(DMUML)+2.0*WRK4)*R(12)+WRK2)	CMNC0023
	BM(11)=2.0*FM-BM11	CMND0024
200	BI=2.0*FM-BI	CMNC0025
	FMT(12)=BI	CMND0026
210	RETURN	CMND0027
220	FM=(S*V(11)/2.+ABSF(DMUML)*BI)/(SGTHV(11)+ABSF(DMUML))	CMND0028
	GCTC200	CMNC0029
	END	CMND0030
*	LABEL	
CZWGHTO		ZWGHT000
	SLBROUTINEZWGHT(BM11)	ZWGHT001
	DIMENSION DMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)	ZWGHT002
	1),BVLZW(8)	ZWGHT003
	DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	ZWGHT004
	DIMENSION R(500),CR(500),V(500),RM(500),SGT-V(500),BM(500),FMT(500)	ZWGHT005
	1),TSN(500)	ZWGHT006
	CCMNCNICEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT	ZWGHT007
	CCMNCNK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4	ZWGHT008
	CCMNCNWRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,BI,S	ZWGHT009
	CCMONDMU,W,F,CVL,BVL,PTTP	ZWGHT010
	CCMNCNTH,SGT,IMAT,NMSH,T	ZWGHT011
	CCMNCNR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW	ZWGHT012
	CCMNCNIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNFT	ZWGHT013
	DMUML=DMU(MC,LC)	ZWGHT014
	WRK1= ABSF(DMUML)*RM(11)	ZWGHT015
	WRK2=0.33333*SGTHV(11)/RM(11)	ZWGHT016
	WRK3=PI	ZWGHT017
	OBI=(S*V(11)+(WRK1-WRK2*(4.*RM(11)-R(12)))*BI)/	ZWGHT018
	1(WRK1+WRK2*(2.0*RM(11)+R(12)))	ZWGHT019
	BM11=(WRK3+BI)/2.0	ZWGHT020
	RETURN	ZWGHT021
	END	ZWGHT022
*	LABEL	
CBVLCYO		BVLCY000
	SLBROUTINEBVLCYL	BVLCY001
	DIMENSION DMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)	BVLCY002
	1),BVLZW(8)	BVLCY003
	DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	BVLCY004
	DIMENSION R(500),CR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500)	BVLCY005
	1),TSN(500)	BVLCY006
	CCMNCNICEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT	BVLCY007
	CCMNCNK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4	BVLCY008
	CCMNCNWRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,BI,S	BVLCY009
	CCMONDMU,W,F,CVL,BVL,PTTP	BVLCY010
	CCMNCNTH,SGT,IMAT,NMSH,T	BVLCY011
	CCMNCNR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW	BVLCY012
	CCMNCNISHIG,ISNH1,ISN1,ISN1G,ICVL,IBVL,IBLCK,NRINIT,PI	BVLCY013
	CCMNCNIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNFT	BVLCY014
	ISN1=ISN+1	BVLCY015
	DC1COLC=1,ISNH	BVLCY016
	J1=ISNHIG-LC	BVLCY017
	DC1COMC=1,J1	BVLCY018
100	CVL(MC,LC)=C.0	BVLCY019
	IF(1BVL-1)145,110,145	BVLCY020
110	DC135LC=1,ISNH	BVLCY021
	J1=ISNHIG-LC	BVLCY022
	DC130MC=2,J1	BVLCY023
	MF=2*J1+1-MC	BVLCY024
130	BVL(MC,LC)=BVL(MP,LC)/(1.0-F(MC,LC))	BVLCY025
135	BVL(1,LC)=BVLZW(LC)/(1.0-F(1,LC))	BVLCY026
	GC TO 300	BVLCY027
145	K1=ISN*(ISN+2)	BVLCY028
	K1=K1/E	BVLCY029
	DC250NT=1,10	BVLCY030
	CC160LC=1,ISNH	BVLCY031
	J1=ISNHIG-LC	BVLCY032
	J2=2*J1-IIGECM	BVLCY033
	J3=J1+1	BVLCY034
	DC150MC=J3,J2	BVLCY035
	MP=2*J1+1-MC	BVLCY036

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150 F(MC,LC)=BVL(MC,LC)+BVL(MP,LC)*F(MP,LC)
160 CCNTINCE
    MCLC=0
    DC220LC=1, ISNH
    J1=ISNH1G-LC
    CC210MC=2, J1
    MCLC=MCLC+1
    LP=1
    K2=0
    WRK1=0.0
    CC200K=1, K1
    K2=K2+1
    IF(ISNH-LP+1-K2)180,190,190
180 K2=1
    LP=LP+1
190 MF=K2+ISNH1G-LP
200 WRK1=WRK1+PTTP(MCLC,K)*F(MP,LP)
210 BVL(MC,LC)=WRK1
220 BVL(1,LC)=BVL(2,LC)
    IF(1BVLP)250,250,225
225 WRITECUTPUTTAPENTOUT,1000,NIT
    CALL MATPT(BVL,17,8,1,ISN1,ISNH,1)
250 CCNTINCE
    IF(ITSNPT)255,300,255
255 WRITECUTPUTTAPENTOUT,1000,NIT
    CALL MATPT(BVL,17,8,1,ISN1,ISNH,1)
300 RETURN
1000 FCRRMAT(29H0BOUNDARY VALUES MATRIX ,NIT=12)
    END
*
    LABEL
CSLABDC
    SLBROUTINESLABBC
    DIMENSION DMU(17,8),w(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)
    1),BVLZW(8)
    DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)
    DIMENSION R(500),DR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500)
    1),TSN(500)
    COMMON IGEOM, ISN, ISNH, MC, LC, NR, IMAX, IMAX1, ATIN, NTOUT
    COMMON K1, K2, K3, K4, J1, J2, J3, J4, I1, I2, I3, I4
    COMMON WRK1, WRK2, WRK3, WRK4, DMUML, WML, GMP, GMP1, BI, S
    COMMON CMU, W, F, CVL, BVL, PTTP
    COMMON TH, SGT, IMAT, NMSH, T
    COMMON NR, DR, V, RM, SGTHV, BM, FMT, TSN, BVLZW
    COMMON ISNH1G, ISNH1, ISN1, ISN1G, ICVL, IBVL, IPLCK, NRINIT, PI
    COMMON IAFPT, ITSNPT, IBVLPT, ICVLPT, ITPT, ISNPT
500 IF(ICVL-1)530,520,505
C
    PERIODIC SLAB
505 DC510MC=1, ISNH
    BVL(MC,1)=CVL(MC,1)/(1.0-F(MC,1))
    MP=ISN1-MC
510 CVL(MP,1)=BVL(MP,1)/(1.0-F(MC,1))
    GCT0560
C
    REFLECTIVE SLAB
520 CC525MC=1, ISNH
    MF=ISN1-MC
    CVL(MP,1)=(CVL(MC,1)+F(MC,1)*BVL(MP,1))/(1.0-F(MC,1)**2)
525 BVL(MC,1)=(BVL(MP,1)+F(MC,1)*CVL(MC,1))/(1.0-F(MC,1)**2)
    GCT0560
C
    BLACK INNER CONDITION
530 DC535MC=1, ISNH
    MF=ISN1-MC
    CVL(MP,1)=0.0
535 BVL(MC,1)=BVL(MP,1)
560 RETURN
    END
*
    LABEL
CTKRNL0
    SLBROUTINETKRNL(IR)
    DIMENSION DMU(17,8),w(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)
    1),BVLZW(8)
    DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)
    DIMENSION R(500),DR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500)
    1),TSN(500)
    COMMON IGEOM, ISN, ISNH, MC, LC, NR, IMAX, IMAX1, ATIN, NTOUT
    COMMON K1, K2, K3, K4, J1, J2, J3, J4, I1, I2, I3, I4
    COMMON WRK1, WRK2, WRK3, WRK4, DMUML, WML, GMP, GMP1, BI, S
    COMMON CMU, W, F, CVL, BVL, PTTP
    COMMON TH, SGT, IMAT, NMSH, T
    COMMON NR, DR, V, RM, SGTHV, BM, FMT, TSN, BVLZW
    COMMON ISNH1G, ISNH1, ISN1, ISN1G, ICVL, IBVL, IPLCK, NRINIT, PI
    COMMON IAFPT, ITSNPT, IBVLPT, ICVLPT, ITPT, ISNPT
    DIMENSION VNR(20)
    IF(ICVL)45,45,50
45 NRINIT=2

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BVLCY037
BVLCY038
BVLCY039
BVLCY040
BVLCY041
BVLCY042
BVLCY043
BVLCY044
BVLCY045
BVLCY046
BVLCY047
BVLCY048
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BVLCY062
BVLCY063
BVLCY064
BVLCY065

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SLABBC00
SLABBC01
SLABBC02
SLABBC03
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SLABBC05
SLABBC06
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TKRNL001
TKRNL002
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TKRNL010
TKRNL011
TKRNL012
TKRNL013
TKRNL014
TKRNL015
TKRNL016
TKRNL017

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<pre> GCTC55 50 NRINIT=1 55 K1=NRINIT K2=NMSH(K1) DC110I=1,IMAX IF(I-K2)100,100,90 90 K1=K1+1 K2=K2+NMSH(K1) 100 IF(IGECM)105,105,108 105 T(IR,K1)=T(IR,K1)+0.5*DR(I)*(TSN(I)+TSN(I+1)) GCTC110 108 T(IR,K1)=T(IR,K1)+DR(I)*(TSN(I+1)*(2.0*R(I+1)+R(I))+TSN(I)*(2.0* R(I)+R(I+1)))/6.0 110 CCNTINUE 160 IF(IR-NR)200,650,200 650 IF(ITPT)655,200,655 655 J2=0 WRITE OUTPUT TAPE NTCUT,3000 CALLMATPT(T,20,20,1,NR,NR,1) DC660I=NRINIT,NR J1=J2+1 J2=J2+NMSH(I) VNR(I)=C.0 DC660J=J1,J2 660 VNR(I)=VNR(I)+V(J) WRITECUTPUTTAPENTOUT,4000 CALLVCTRPT(1,VNR,NR,2) DC680I=NRINIT,NR WRK1=C.C DC670J=NRINIT,NR K2=IMAT(J) T(I,J)=SGT(K2)*T(I,J)/VNR(I) 670 WRK1=WRK1+T(I,J) IF(IBVL)200,680,675 675 WRITE OUTPUT TAPE NTCUT,1000,1,WRK1 680 CCNTINUE WRITECUTPUTTAPENTOUT,2000 CALLMATPT(T,20,20,1,NR,NR,1) 200 RETURN 1000 FCRMAT(16HCSUM OVER J OF P,13,4H J=E12.5) 2000 FCRMAT(29HOCOLLISION PROBABILITY MATRIX) 3000 FCRMAT(21HCMATRIX PIJ=LAMDAJ*VI//) 4000 FCRMAT(18HOVOLUME OF REGIONS) END * LABEL CMESH=CO SLBROUTINEMESH DIMENSION DMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36 1),BVLZW(8) DIMENSION TF(20),SGT(20),IMAT(20),NMSH(20),T(20,20) DIMENSION R(500),CR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500) 1),TSN(500) COMMONICEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT COMMONK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4 COMMONWRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,B1,S COMMONCMU,W,F,CVL,BVL,PTTP COMMONTF,SGT,IMAT,NMSH,T COMMONR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW COMMONISNH1C,ISNH1,ISN1,ISN1G,ICVL,IBVL,IBLCK,NRINIT,PI COMMONIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNPT DIMENSIONBMSH(20),CMST(20) READ INPUT TAPE 5,1004,A,B,C MSHMX=500 IF(IGECM)75,75,50 50 IF(ICVL)60,60,75 60 NRINIT=2 R(1)=TF(1) GCTC8C 75 NRINIT=1 R(1)=C.C 80 DC130K1=NRINIT,NR WRK1=TF(K1) K2=IMAT(K1) WRK2=1./SGT(K2) WRK3=WRK2/A WRK4=WRK1/B IF(WRK3-WRK4)100,110,110 100 CMST(K1)=WRK3 GCTC115 110 CMST(K1)=WRK4 115 WRK3=WRK2/C WRK4=WRK1/2. IF(WRK3-WRK4)120,130,130 120 BMSH(K1)=WRK3 </pre>	<pre> TKRNL018 TKRNL019 TKRNL020 TKRNL021 TKRNL022 TKRNL023 TKRNL024 TKRNL025 TKRNL026 TKRNL027 TKRNL028 TKRNL029 TKRNL030 TKRNL031 TKRNL032 TKRNL033 TKRNL034 TKRNL035 TKRNL036 TKRNL037 TKRNL038 TKRNL039 TKRNL040 TKRNL041 TKRNL042 TKRNL043 TKRNL044 TKRNL045 TKRNL046 TKRNL047 TKRNL048 TKRNL049 TKRNL050 TKRNL051 TKRNL052 TKRNL053 TKRNL054 TKRNL055 TKRNL056 TKRNL057 TKRNL058 TKRNL059 TKRNL060 TKRNL061 MESH0000 MESH0001 MESH0002 MESH0003 MESH0004 MESH0005 MESH0006 MESH0007 MESH0008 MESH0009 MESH0010 MESH0011 MESH0012 MESH0013 MESH0014 MESH0015 MESH0016 MESH0017 MESH0018 MESH0019 MESH0020 MESH0021 MESH0022 MESH0023 MESH0024 MESH0025 MESH0026 MESH0027 MESH0028 MESH0029 MESH0030 MESH0031 MESH0032 MESH0033 MESH0034 MESH0035 MESH0036 MESH0037 MESH0038 </pre>
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GCTC131	MESH0039
130 BMSH(K1)=WRK4	MESH0040
131 IMSH=1	MESH0041
XR2=R(1)	MESH0042
YR2=CMSH(INRINIT)	MESH0043
XR1=XR2	MESH0044
YR1=YR2	MESH0045
X=R(1)	MESH0046
DRC=CMSH(INRINIT)	MESH0047
CC260K=NRINIT, NR	MESH0048
K2=0	MESH0049
K3=IMAT(K)	MESH0050
XL1=XR1	MESH0051
XL2=XR2	MESH0052
YL1=YR1	MESH0053
YL2=YR2	MESH0054
WRK1=R(IMSH)	MESH0055
WRK2=WRK1+T(K)	MESH0056
IF(K-NR)135,1352,1352	MESH0057
135 YR1=YR2	MESH0058
YR2=CMSH(K+1)	MESH0059
IF(YR2-YR1)1351,1352,1353	MESH0060
1351 XR1=WRK2-BMSH(K)	MESH0061
XR2=WRK2	MESH0062
GCTC137	MESH0063
1352 XR1=WRK2	MESH0064
XR2=WRK2	MESH0065
GCTC137	MESH0066
1353 XR1=WRK2	MESH0067
XR2=WRK2+BMSH(K+1)	MESH0068
137 K1=1	MESH0069
140 IMSH=IMSH1	MESH0070
IMSH=IMSH+1	MESH0071
IF(IMSHX-IMSH)270,270,145	MESH0072
145 K2=K2+1	MESH0073
IF(X-XL2)15C,170,17C	MESH0074
150 DRC=RLINK(XL1,YL1,XL2,YL2,X)	MESH0075
GCTC250	MESH0076
170 IF(X-XR1)175,175,190	MESH0077
175 IF(XR1-WRK2)180,176,190	MESH0078
176 IF(X-XR1+0.2*DRC)180,210,210	MESH0079
180 DRC=CMSH(K)	MESH0080
GCTC250	MESH0081
190 IF(X-WRK2+0.2*DRC)200,210,210	MESH0082
200 DRC=RLINK(XR1,YR1,XR2,YR2,X)	MESH0083
GCTC250	MESH0084
210 X=WRK2	MESH0085
IMSH=IMSH	MESH0086
IMSH=IMSH-1	MESH0087
DRC=X-R(IMSH)	MESH0088
K1=2	MESH0089
K2=K2-1	MESH0090
GCTC251	MESH0091
250 X=X+DRC	MESH0092
251 R(IMSH)=X	MESH0093
WRK3=(R(IMSH)+R(IMSH))/2.0	MESH0094
IF(IGEOM)253,253,254	MESH0095
253 V(IMSH)=DRC	MESH0096
GCTC255	MESH0097
254 V(IMSH)=DRC*WRK3	MESH0098
255 RM(IMSH)=WRK3	MESH0099
SGTHV(IMSH)=SGT(K3)*V(IMSH)/2.	MESH0100
DRC(IMSH)=DRC	MESH0101
GCTC(14C,257),K1	MESH0102
257 NMSH(K)=K2	MESH0103
260 CCNTINUE	MESH0104
IMAX=IMSH	MESH0105
IMAX1=IMSH1	MESH0106
IF(ITSNFT)265,265,262	MESH0107
262 WRITECUTPUTTAPENTOUT,1002	MESH0108
WRITECUTPUTTAPENTOUT,1003	MESH0109
OCALLPRINT(8,R,IMAX1,2,DR,IMAX,2,RP,IMAX,2,V,IPAX,2,NMSH,AR,1,CMSH,	MESH0110
INR,2,BMSH,NR,2,SGTHV,IMAX,2)	MESH0111
265 RETURN	MESH0112
270 WRITECUTPUTTAPE6,1001	MESH0113
CALLEXIT	MESH0114
1001 FCRMAT(21H TOO MUCH MESH POINTS)	MESH0115
1002 FCRMAT(1H151X16HGEOMETRICAL MESH//)	MESH0116
1003 FCRMAT(///11X6HRAC1US8X6HCELTAR8X6HR-PEAN8X6HVOLUME//)	MESH0117
1004 FCRMAT(3E12,5)	MESH0118
END	MESH0119
* LABEL	
RLINK0	RLINK000
FLNCTICARLINK(X1,Y1,X2,Y2,X)	RLINK001

CSNWCTO	SLBROUTINESWGT	SNWGT000
	SA DIRECTICA MESH AND WEIGHTS FOR N=2,4,6,8,12OR16	SNWGT001
C	DIMENSION CMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36	SNWGT002
	1),BVLZW(8)	SNWGT003
	DIMENSION T(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	SNWGT004
	DIMENSION R(500),CR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500	SNWGT005
	1),TSN(500)	SNWGT006
	COMMON GEOM, ISN, ISNH, MC, LC, NR, IMAX, IMAX1, NTIN, NTOUT	SNWGT007
	COMMON K1, K2, K3, K4, J1, J2, J3, J4, I1, I2, I3, I4	SNWGT008
	COMMON WRK1, WRK2, WRK3, WRK4, CMUML, WML, GMP, GMP1, BI, S	SNWGT009
	COMMON CMU, W, F, CVL, BVL, PTTP	SNWGT010
	COMMON T, SGT, IMAT, NMSH, T	SNWGT011
	COMMON DR, V, RM, SGTHV, BM, FMT, TSN, BVLZW	SNWGT012
	COMMON ISNH1G, ISNH1, ISN1, ISN1G, ICVL, IBVL, IBLCK, NRINIT, PI	SNWGT013
	COMMON IAFPT, ITSNT, IBVLPT, ICVLPT, ITPT, ISNPT	SNWGT014
	DIMENSION P(8)	SNWGT015
	XSABF(I)=2*K3+1-I+2*IGE	SNWGT016
	XSAMF(I)=K3+1-I+2*IGE	SNWGT017
	XTBCF(I)=K3+1	SNWGT018
15	IF(IGECM)16,16,17	SNWGT019
16	IGE=0	SNWGT020
	GCTC18	SNWGT021
17	IGE=1	SNWGT022
18	ISNH=ISN/2	SNWGT023
	ISNH1=ISNH+1	SNWGT024
	ISN1=ISN+1	SNWGT025
	ISNH1G=ISNH+1+IGE	SNWGT026
	ISN1G=ISN+1+IGE	SNWGT027
	ISNH1G=ISNH+IGE	SNWGT028
	ISNG=ISN+IGE	SNWGT029
	CC150J=1, ISNH	SNWGT030
	CC150I=1, ISN1	SNWGT031
	W(I,J)=C.0	SNWGT032
150	CMU(I,J)=0.C	SNWGT033
	IF(ISNH-912C0,555,555	SNWGT034
C	PREPARATION OF COSML	SNWGT035
200	CC260 L=1, ISNH	SNWGT036
	J1=ISNH-1-L	SNWGT037
	CC250 M=1, J1	SNWGT038
	K=J1+1-M	SNWGT039
	MC=M+IGE	SNWGT040
	X= (6.*FLOATF(K)-5.)/(3.*(FLOATF(ISN)-1.))	SNWGT041
	X=-SQRTF(X)	SNWGT042
	CMU(MC,L)=X	SNWGT043
210	K=2*J1+1-M+IGE	SNWGT044
	DMU(K,L)=-X	SNWGT045
250	CCNTINUE	SNWGT046
	IF(IGECM)260,270,255	SNWGT047
255	DMU(I,L)=-SQRTF(1.-DMU(MD,1)**2)	SNWGT048
260	CCNTINUE	SNWGT049
270	GCTC(30C,31C,320,330,555,350,555,37C),ISNH	SNWGT050
C	S2 WEIGHTS	SNWGT051
300	P(1)=C.5	SNWGT052
	GCTC500	SNWGT053
C	S4 WEIGHTS	SNWGT054
310	P(1)=0.16666667	SNWGT055
	GCTC500	SNWGT056
C	S6 WEIGHTS	SNWGT057
320	P(1)=C.08043063	SNWGT058
	P(2)=C.08623605	SNWGT059
	GCTC500	SNWGT060
C	S8 WEIGHTS	SNWGT061
330	P(1)=C.05330038	SNWGT062
	P(2)=C.05058636	SNWGT063
	P(3)=C.03658070	SNWGT064
	GCTC500	SNWGT065
C	S12 WEIGHTS	SNWGT066
350	P(1)=C.03188428	SNWGT067
	P(2)=C.02844993	SNWGT068
	P(3)=C.02268799	SNWGT069
	P(4)=C.01736872	SNWGT070
	P(5)=C.01513782	SNWGT071
	GCTC500	SNWGT072
C	S16 WEIGHTS	SNWGT073
370	P(1)=C.02275580	SNWGT074
	P(2)=C.01988730	SNWGT075
	P(3)=C.01502308	SNWGT076
	P(4)=C.01366597	SNWGT077
	P(5)=C.01164258	SNWGT078
	P(6)=C.00931431	SNWGT079
	P(7)=C.00881570	SNWGT080
	P(8)=C.00767130	SNWGT081
500	J3=0	SNWGT082
		SNWGT083

	CC530 L=1, ISNH	SNWGT084
	J1=ISNH-1-L	SNWGT085
	J2=J1/2	SNWGT086
	IF(J1-2*J2)503,503,502	SNWGT087
502	J2=J2+1	SNWGT088
503	DC520 M=1, J2	SNWGT089
	M=M	SNWGT090
	MC=M+IGE	SNWGT091
	IF(W(MC,L))520,510,520	SNWGT092
510	J3=J3+1	SNWGT093
	X=P(J3)	SNWGT094
	K2=0	SNWGT095
511	K2=K2+1	SNWGT096
	GCTO(5111,5113,5115,520),K2	SNWGT097
5111	MP=M+IGE	SNWGT098
	LF=L	SNWGT099
	GCTO513	SNWGT100
5113	LP=M	SNWGT101
	GCTO512	SNWGT102
5115	LP=J1+1-M	SNWGT103
512	MP=L+IGE	SNWGT104
513	K1=0	SNWGT105
	MC=MP	SNWGT106
	K3=ISNH-1-LP	SNWGT107
514	K1=K1+1	SNWGT108
	W(MP,LP)=X	SNWGT109
	GCTC(515,516,517,511),K1	SNWGT110
515	MP=XSABF(MD)	SNWGT111
	GCTO514	SNWGT112
516	MP=XSAMF(MC)	SNWGT113
	GCTO514	SNWGT114
517	MF=XTRCF(MC)	SNWGT115
	GCTO514	SNWGT116
520	CCNTINUE	SNWGT117
530	CCNTINUE	SNWGT118
	IF(IGECM)540,531,540	SNWGT119
531	CC538M=2, ISNH	SNWGT120
	WRK1=C.C	SNWGT121
	DC535L=2, M	SNWGT122
	MC=M-L+1	SNWGT123
	WRK1=WRK1 +W(MC,L)	SNWGT124
	W(MC,L)=0.0	SNWGT125
	DMU(MC,L)=0.0	SNWGT126
	K3=ISNH-1-L	SNWGT127
	MP=XSABF(MD)	SNWGT128
	W(MP,L)=0.0	SNWGT129
535	DMU(MP,L)=0.0	SNWGT130
	W(M,1)=W(M,1)+WRK1	SNWGT131
	MP=ISNH-M	SNWGT132
538	W(MP,1)=W(M,1)	SNWGT133
540	IF(ISNPT)543,543,542	SNWGT134
542	WRITECLTPUTTAPENTOLT,1000,ISN	SNWGT135
	CC545LC=1, ISNH	SNWGT136
	J1=ISN-2*(LC-1)+IGE	SNWGT137
	WRITECUTPUTTAPENTOUT,1001,(M,LC,DMU(M,LC),W(M,LC),M=1,J1)	SNWGT138
543	IF(IGECM)545,550,545	SNWGT139
545	CCNTINUE	SNWGT140
550	RETURN	SNWGT141
555	WRITECLTPUTTAPENTOUT,1002,ISN	SNWGT142
	CALLEXIT	SNWGT143
1000	FCRMT(1H149X19HANGULAR SN MESH (N=12,1F)//45X3HPML10X4HPUML11X3HW	SNWGT144
	1ML//)	SNWGT145
1001	FCRMT(44X1HP212,3X2E14.5)	SNWGT146
1002	FCRMT(25H SN WEIGHTS ARE NOT PROVIDED FOR N=[4]	SNWGT147
	END	SNWGT148
	LABEL	
CPRINT0	SUBROUTINEPRINT(NITEM,V1,L1,IT1,V2,L2,IT2,V3,L3,IT3,V4,L4,IT4,V5,L	PRINT000
	15,IT5,V6,L6,IT6,V7,L7,IT7,V8,L8,IT8)	PRINT001
	DIMENSICNV1(1),V2(1),V3(1),V4(1),V5(1),V6(1),V7(1),V8(1)	PRINT002
	DIMENSICNFORMAT(9),VLIN(E)	PRINT003
C	BLILT-IN FORMATS	PRINT004
	FCRMT(1)=6F(2X14,	PRINT005
	FMTFX1=6H7X,17,	PRINT006
	FMTFX2=6H7X,17)	PRINT007
	FMTFL1=6HE14.5,	PRINT008
	FMTFL2=6HE14.5)	PRINT009
	FMTBK1=6H13XA1,	PRINT010
	FMTBK2=6H13XA1)	PRINT011
B	BLANK=6C606C606060	PRINT012
	WRITE CLTPUT TAPE 6,1000,(1,I=1,NITEM)	PRINT013
	LINC=0	PRINT014
S	K=0	PRINT015
C	FCRMT CF LINE	PRINT016
		PRINT017

```

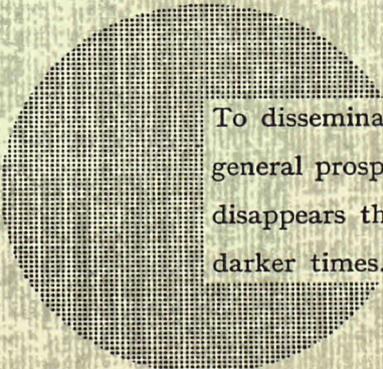
LINC=LINO+1
CC2501=1,NITEM
GCTC(10,20,30,40,50,60,70,80),I
10 ITYPE=I11
   LENGTH=L1
B   VAR=V1(LINO)
   GCTC10C
20 ITYPE=I12
   LENGTH=L2
B   VAR=V2(LINO)
   GCTC10C
30 ITYPE=I13
   LENGTH=L3
B   VAR=V3(LINO)
   GCTC10C
40 ITYPE=I14
   LENGTH=L4
B   VAR=V4(LINO)
   GCTC10C
50 ITYPE=I15
   LENGTH=L5
B   VAR=V5(LINO)
   GCTC10C
60 ITYPE=I16
   LENGTH=L6
B   VAR=V6(LINO)
   GCTC10C
70 ITYPE=I17
   LENGTH=L7
B   VAR=V7(LINO)
   GCTC10C
80 ITYPE=I18
   LENGTH=L8
B   VAR=V8(LINO)
100 IF(LINO-LENGTH)150,150,200
150 GCTC(16C,17C),ITYPE
160 IF(I-8)162,165,165
162 FMT=FMTFX1
   GCTC20C
165 FMT=FMTFX2
   GCTC20C
170 IF(I-8)172,175,175
172 FMT=FMTFL1
   GCTC20C
175 FMT=FMTFL2
   GCTC20C
200 K=K+1
   IF(I-8)202,205,205
202 FMT=FMTEK1
   GCTC20C
205 FMT=FMTEK2
207 VAR=BLANK
208 FCRMAT(I+1)=FMT
   VLINE(I)=VAR
   MF=I
250 CCNTINUE
   IF(MP-8)260,280,2E0
260 MP=MP+1
   CC270I=MP,8
   FCRMAT(I+1)=FMTEK1
270 VLINE(I)=BLANK
   FCRMAT(5)=FMTEK2
280 IF(K-NITEM)300,290,290
290 RETURN
300 WRITEOUTPUTTAPE6,FORMAT,LINO,(VLINE(I),I=1,8)
   GCTO5
1000 FCRMAT(1H013X11,7I14)
   END

```

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PRINT018
PRINT019
PRINT020
PRINT021
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PRINT085

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To disseminate knowledge is to disseminate prosperity — I mean general prosperity and not individual riches — and with prosperity disappears the greater part of the evil which is our heritage from darker times.

Alfred Nobel

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